

Drilled shaft to resist Overturning

This application perform to calculate the required depth of Drilled shaft to prevent overtuning based on AASHTO LRFD (Load and Resistance Factor Design).

References:

- AASHTO LRFD Specification for Structural Supports for Highway Signs, Luminaires and Traffic Signals
- AASHTO LRFD Bridge Design Specification
- [FDOT Structures Manual](#)

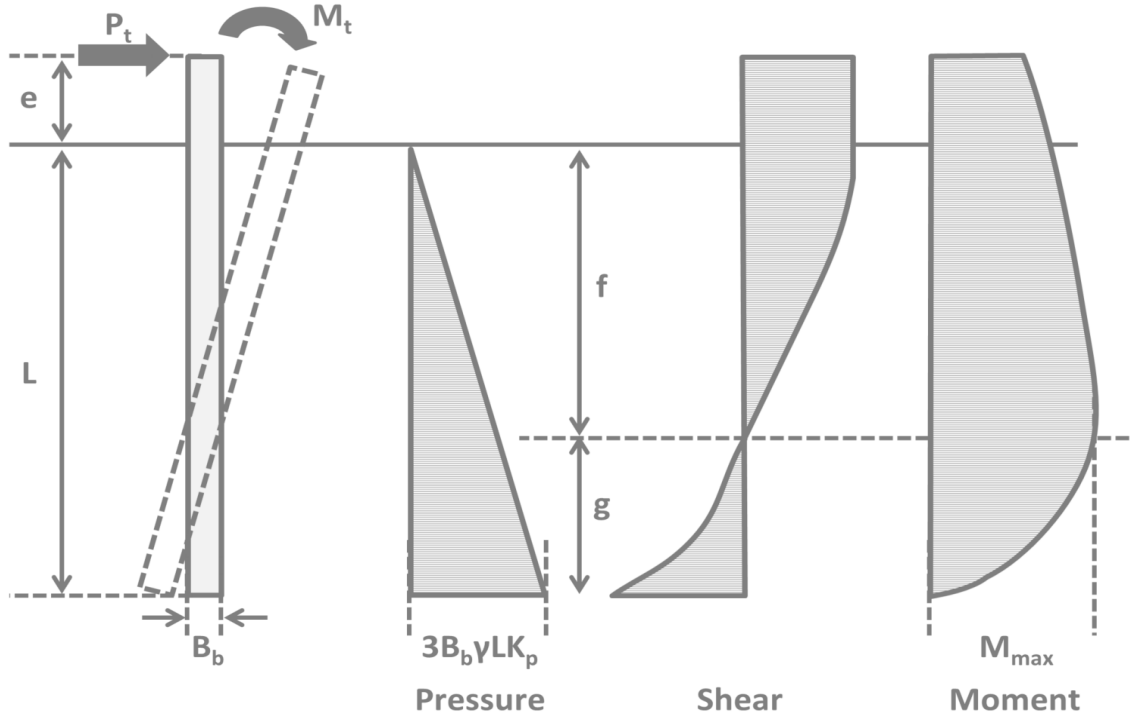


Figure 1 : Broms Pressure, Shear, Moment diagram for Cohesionless soils

Design parameters

Soil properties

- Soil friction angle $\phi_s := 32 \text{ deg}$
- Soil shear strength $c_s := 15 \text{ psi}$
- Effective soil weight $\gamma_s := 60 \frac{\text{lbf}}{\text{ft}^3}$

Geometrical parameters

Diameter of shaft $B_b := 4.0 \text{ ft}$

Groupline to top of foundation $\text{Offset} := 0.0 \text{ ft}$

Applied loads

Force of X-direction $V_x := 40 \text{ kip}$

Force of Z-direction $V_z := 25.0 \text{ kip}$

Moment of X-direction $M_x := 250 \text{ kip}\cdot\text{ft}$

Moment of Z-direction $M_z := 1075 \text{ kip}\cdot\text{ft}$

Torsional load $T_{\text{load}} := 150 \text{ kip}\cdot\text{ft}$

Overturning factor $\phi_{\text{ot}} := 0.6$

Torsional load factor $\phi_{\text{tor}} := 0.9$

Load moment and force

Design load moment $M_t := \sqrt{M_x^2 + M_z^2} = 1103.687 \text{ kip foot}$

Design load force $P_t := \sqrt{V_x^2 + V_z^2} = 47.170 \text{ kip}$

Design torsional force (Torque) $T_t := T_{\text{load}} = 150 \text{ kip}\cdot\text{foot}$

Cohesionless soil (Sand)

Rankine coefficient of
passive earth pressure

$$K_p := \tan\left(45 \cdot \text{deg} + \frac{\phi_s}{2}\right)^2 = 3.255$$

Top of shaft to the ground

$$e_s := \text{Offset} = 0.$$

Objective function to obtain the minimum length of the shaft

$$\text{Obj}_s := P_t \cdot (e_s + L_{\text{min}_s}) + M_t = \phi_{\text{ot}} \cdot (3 \cdot \gamma_s \cdot B_b \cdot L_{\text{min}_s} \cdot K_p) \cdot \left(\frac{1}{2} \cdot L_{\text{min}_s}\right) \cdot \left(\frac{1}{3} \cdot L_{\text{min}_s}\right)$$

$$L_s := \text{fsolve}(\text{Obj}_s) = 20.707 \text{ ft}$$

Depth, Point of zero shear and Point of
Maximum moment

$$f_s := \sqrt{\frac{P_t}{1.5 \cdot B_b \cdot \gamma_s \cdot K_p \cdot \phi_{\text{ot}}}} = 8.191 \text{ ft}$$

Maximum moment

$$M_{\text{max}_s} := M_t + P_t \cdot (e_s + f_s) - \frac{1}{2} \cdot B_b \cdot \gamma_s \cdot f_s^3 \cdot K_p \cdot \phi_{\text{ot}} = 1361.278 \text{ kip foot}$$

Cohesive soil (Clay, $L > 3 \cdot B_b$)

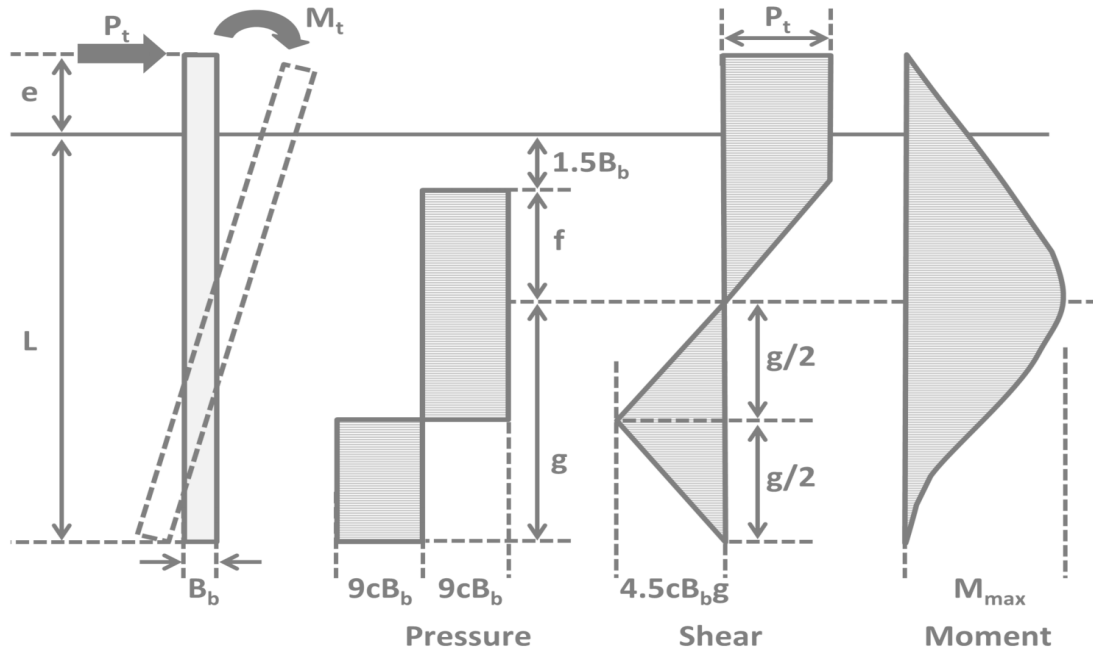


Figure 2 : Broms Pressure, Shear, Moment diagram for Cohesive soils

Soil shear strength
to avoid division-by-zero

$$c_s := \begin{cases} 0 \frac{\text{lbf}}{\text{ft}^2} & c_s = 0.0 \frac{\text{lbf}}{\text{ft}^2} \\ c_s & \text{otherwise} \end{cases}$$

Depth, Point of zero shear and Point of Maximum moment

$$f := \frac{P_t}{\phi_{ot} \cdot 9 \cdot c_s \cdot B_b} = 12.132 \text{ in}$$

Maximum moment

$$M_{\text{max}_c} := P_t \cdot \left(\frac{M_t}{P_t} + \text{Offset} \right) + \frac{3}{2} \cdot P_t \cdot B_b \cdot f + \frac{1}{2} \cdot P_t \cdot f^2 = 1410.551 \text{ kip foot}$$

Depth, Point of zero shear and Point of Maximum moment

$$g := \sqrt{\frac{2 \cdot M_{\text{max}_c}}{4.5 \cdot \phi_{ot} \cdot c_s \cdot B_b}} = 10.997 \text{ ft}$$

Minimum length

$$L_c := 1.5 \cdot B_b + f + g = 18.008 \text{ ft}$$